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Power in sports

A literature review on the application, assumptions, and terminology of mechanical power in sport research

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POWER IN SPORTS: A LITERATURE REVIEW ON THE APPLICATION, ASSUMPTIONS, AND TERMINOLOGY OF MECHANICAL POWER IN SPORT RESEARCH.

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Key words: mechanical power, internal power, external power, mechanical energy expenditure, joint power

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Power in Sports: a literature review on the application, assumptions, and terminology of mechanical power in sport research.

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10 Abstract

The quantification of mechanical power can provide valuable insight into athlete performance 11 12 because it is the mechanical principle of the rate at which the athlete does work or transfers energy to 13 complete a movement task. Estimates of power are usually limited by the capabilities of 14 measurement systems, resulting in the use of simplified power models. This review provides a 15 systematic overview of the studies on mechanical power in sports, discussing the application and 16 estimation of mechanical power, the consequences of simplifications, and the terminology. The 17 mechanical power balance consists of five parts, where joint power is equal to the sum of kinetic 18 power, gravitational power, environmental power, and frictional power. Structuring literature based 19 on these power components shows that simplifications in models are done on four levels, single vs 20 multibody models, instantaneous power (IN) versus change in energy (EN), the dimensions of a model 21 (1D, 2D, 3D), and neglecting parts of the mechanical power balance. Quantifying the consequences 22 of simplification of power models has only been done for running, and shows differences ranging from 23 10% up to 250% compared to joint power models. Furthermore, inconsistency and imprecision were 24 found in the determination of joint power, resulting from inverse dynamics methods, incorporation of 25 translational joint powers, partitioning in negative and positive work, and power flow between 26 segments. Most inconsistency in terminology was found in the definition and application of 'external' 27 and 'internal' work and power. Sport research would benefit from structuring the research on 28 mechanical power in sports and quantifying the result of simplifications in mechanical power 29 estimations.

Glossary power terminology

- work work done by a system is the energy transferred from that system to the surrounding
- energy the quantitative property that must be transferred to an object in order to perform work on it
- power the rate of work, the amount of energy generated or transferred per unit time.
- Joint power the mechanical power generated by the human at $\frac{N-1}{2}$

the joints
$$P_j = \sum_{i=1}^{j} M_{i,i+1} \cdot (\omega_{i+1} - \omega_i) = \sum_{j=1}^{j} M_j \cdot \omega_j$$

Kinetic power the rate of change of the kinetic energy $P_k = \sum \frac{dE_{wg}}{dt} = \sum_{i=1}^{N} \frac{d}{dt} (l_i \omega_i) \cdot \omega_i + \sum_{i=1}^{N} m_i \cdot a_i \cdot v_i$

Gravitational power the rate of change of the gravitational en- $\frac{N}{N}$

ergy
$$P_G = \sum_{i=1} v_i \cdot m_i \cdot g$$

Environmental power the mechanical power from external ap-

plied forces and moments.
$$P_e = \sum_{i=1}^{n} \omega_i \cdot M_{e,i} + \dots$$

 $\sum_{i=1}^{n} v_i \cdot F_{e,i} We$ here use the term environmental power to

avoid the term external power which has been used to describe several different models (see section 5.2.1) Frictional power the power loss from the frictional forces (e.g. air

riction, roll friction)
$$P_f = \sum_{i=1}^{N} \omega_i \cdot M_{fr,i} + \sum_{i=1}^{N} v_i \cdot F_{fr,i}$$

Mechanical power balance the mechanical power balance consists of five parts: joint power, kinetic power, gravitational power, environmental power, and frictional power, $P_i = P_k + P_f - P_G - P_e$

Validity the process of determining the degree to which a model is an accurate representation of the real world from the perspective of the intended uses of the model (Thacker, 2001)

Technique factors variables in the movement coordination of an athlete

Mechanical power in human movement can be determined by applying the laws of classic mechanics to the human body, and by modelling it as a linked segment model consisting of several bodies

Muscle power the rate at which a muscle does work or transfers energy to complete a movement task

Metabolic power metabolic work per unit time

- Metabolic work the amount of energy used by a human (during a movement task) (metabolic approach); Metabolic work can be measured by the rate of oxygen uptake, from which the energy expenditure for the complete body is estimated.
- Mechanical energy expenditure The amount of energy used by an athlete to complete a movement task based on the mechanical power balance
- Single body The human is simplified to a single mass model Multibody The human is modelled as a number of rigid bodies connected by idealized joints
- Instantaneous power (IN) power at any instant of time, which can be calculated using the mechanical power balance equation
- Change of energy (EN) Power, $\Delta E/\Delta t$, which is estimated by determining the change of kinetic and gravitational energy of a system ΔE over a larger time span Δt , e.g. the cycle time, and divide by Δt .
- Kinematic approach In the kinematic approach, only recorded kinematic data are used to estimate mechanical power.
- Joint power: Single joint joint power of an individual joint is estimated
- Joint power: Multiple joints in these researches the joint power is estimated over multiple joints

Internal power See peripheral power

External power See environmental power

- Peripheral power Power due to moving body segments relative to the COM (Zelik & Kuo 2012; Riddick & Kuo 2016). Only to be used when the power due to motion of the COM and due to motion of the segments relative to the COM are to be separated for measurement conveniences. Note however, that peripheral power and environmental power should not be interpreted as separate energy measures (mechanical work).
- Maintenance power the rate at which energy is used to maintain the body processes
- Entropy Represents the loss of energy to heat dissipation Non-conservative power Power from an irreversible process like
- heat dissipation, negative work, frictional work. Conservative power power due to conservative forces, which in principle can be re-used such as with tendon stretch
- E-gross is the ratio between the expended work (metabolic work) and the performed work (mechanical work)

Positive work Work done by muscles to accelerate the motion. Negative work Work done by muscles to decelerate the motion.

non-regenerative work.

30

31 **1. Introduction**

Mechanical power is a metric often used by sport scientists, athletes, and coaches for research and 32 33 training purposes. Mechanical power is the mechanical principle of the rate at which the athlete does 34 work or transfers energy to complete a movement task. A mechanical power balance analysis can 35 provide valuable insight in the capability of athletes to generate power, and also in technique factors 36 affecting the effective use of power for performance. The estimates of mechanical power are usually 37 limited by the capabilities of motion capture systems, resulting in the necessity to use simplified 38 power models. However, due to the introduction of these simplified models and thus variation in 39 how power is calculated, the overview in literature in the terminology and estimation of mechanical 40 power is disordered. Furthermore, the validity of the simplifications is often disregarded. 41 The inconsistency in the use and definition of power came to our attention, when attempting to 42 estimate the mechanical power balance in speed skating (Winter et al. 2016; van der Kruk 2018). 43 Although thorough reviews exist addressing the issues of the mechanical power equations (van Ingen Schenau & Cavanagh 1990; Aleshinsky 1986) and mechanical efficiency (van Ingen Schenau & 44 Cavanagh 1990), we found inconsistencies in the (post 1990) literature on the power estimations 45 and terminology. Moreover, the quantification on consequences of simplifications has usually been 46

- 48 hampers interpretation and comparison to the literature. Providing insight into the interrelations
- 49 between the different models, estimations, and assumptions can benefit the interpretation of power
- 50 results and assist scientists in performing power estimations which are appropriate for their specific
- 51 applications.
- 52 The aim of this study is to provide an overview of the existing papers on mechanical power in sports,
- 53 discussing its application and estimation, consequences of simplifications, and terminology.
- 54
- 55

56 **2. Method**

57 A literature search was carried out in July 2017 in the database Scopus. The keywords "mechanical 58 power" and "sport" were used in the search (128 articles) (Search 1). The search was limited to 59 papers in English. Abstracts of the retrieved papers were read to verify whether the article was 60 suited to the aim of the paper, papers that estimated 'power' for a sporting exercise were included 61 (resulting in 94 articles). Three additional searches were performed in August 2017 addressing three specific power estimations, combining the keyword "sport" with "external power" (30 articles) 62 63 (Search 2), "internal power" (4 articles) (Search 3), and "joint power" (35 articles) (Search 4), 64 restricted to articles published after 1990. Again, the abstracts of the retrieved papers were read to 65 verify whether the papers were suited for the current review. Papers that estimated 'power' for a sporting exercise were included (resulting in respectively 13, 3, and 26 articles). 66

67 **3. Application of the term power**

68 When the terms *mechanical power* and *sport* were used in articles, the scope of the papers can 69 roughly be divided into two categories: the term power was either used as a strength characteristic 70 or performance measure (approximately 75% of the articles), or as an indication of mechanical 71 energy expenditure *(MEE)* (muscle work), which we focus on in this review. 72 The first application was mainly found in fitness and strength studies. Power is then wrongly used as 73 a strength measure, attributed to a certain athlete (Winter et al. 2016). This would implicate that 74 (peak) mechanical power is a synonym for short-term, high intensity neuromuscular performance 75 characteristic, which is directly related to performance of an athlete. However, as Knudson (2009) 76 also discusses, a peak power is not a fixed characteristic of a certain athlete. The power estimation in 77 a certain exercise, e.g. the well-known vertical jump (Bosco et al. 1983), cannot be directly translated 78 into performance of an athlete for other movements. Secondly, while strength is a force 79 measurement, power is a combination of force and velocity (Minetti 2002); these two are not 80 interchangeable.

81 Power can of course be used as an *indication of performance* during endurance sports. In cycling 82 practices, power meters (e.g., SRM systems, Schoberer Rad Messtechnik, Welldorf, Germany) are 83 widely accepted and used as an indication of the intensity of the training or race. Since a SRM system 84 determines power as the product of pedal force and rotational velocity of the sprocket, under the 85 same conditions (e.g. equal frictional and gravitational forces), the cyclist with the highest generated 86 power per body weight over time (work) will be fastest. This is, however, not applicable for every 87 sport. For example, power generated by a skater not only generates a forward motion (in line with 88 the rink), but also a lateral one (perpendicular to the rink). The result of this being that the skater 89 that generates the most power is not necessarily the fastest one finishing. Technique factors will 90 determine the effectiveness of the generated power towards propulsion. 91 This review focuses on the second purpose of power estimation: as indication of mechanical energy 92 expenditure (MEE). Power is the rate of doing work, the amount of energy transferred per unit time. 93 The relationship between mechanical power, muscle power and metabolic power is shown in Figure 94 1. Metabolic power can be measured by the rate of oxygen uptake, from which the energy

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95 expenditure for the complete body in time is estimated. Mechanical power can be determined by 96 applying the laws of classic mechanics to the human body, and by modelling it as a linked segment 97 model consisting of several bodies (Aleshinsky 1986). Both metabolic power and mechanical power 98 estimates eventually aim to approach muscle power (either via the metabolic or via the mechanical 99 approach). Although muscle work is closely related to the MEE for the movement, mechanical power 100 and work are far from an exact estimation of muscle power and work and thus from MEE. 101 The disparity between mechanical power and muscle power can, next to measurement inaccuracies, 102 be attributed to physiological factors. In a mechanical approach, the part of the muscle power which 103 is degraded into heat or non-conservative frictional forces inside the body or in antagonistic co-104 contraction is not taken into account (Figure 1). Neither is the power against conservative forces 105 taken into account, such as tendon stretch, which in principle can be re-used (van Ingen Schenau & 106 Cavanagh 1990).

107



108

mechanical power balance

109 Figure 1 The power flow in human movement. Metabolic power and work are a chemical process, estimated by 110 for example measuring lactate or oxygen uptake (a). Energy distributes into muscle power, maintenance power 111 and entropy. Muscle power results in mechanical power (force times contraction velocity), except for non-112 conservative power (e.g., power due to heat dissipation, non-conservative frictional forces inside the body, or 113 when muscles work against each other) and conservative power (e.g. power due to conservative forces, which in 114 principle can be re-used such as with tendon stretch). It is possible to convert the mechanical power into an 115 actual estimation of muscle power by the use of musculoskeletal models (II). The mechanical power balance 116 consists of joint power, which is generated by the human, which results in the kinetic power, which is the rate of 117 change of the kinetic energy, frictional power, due to e.g. air resistance, environmental power, which is induced 118 by external forces and moments, and gravitational power. The mechanical power can therefore be estimated 119 by the joint power alone, or by the combination of kinetic, frictional, environmental and gravitational power. E-120 gross is the ratio between the expended work (metabolic work) and the performed work (mechanical work).

121



122 123 Figure 2 Free body diagram of a rigid segment model of a human (adopted from van der Kruk et al. (2018)). The 124 human body is here divided into eight segments; the feet (f), the legs (e), the thighs (t), the pelvis (p) and a HAT 125 (h), which are the head-arms-trunk. Note that HAT can only be appropriately grouped for certain sports 126 activities (such as ones that focus on lower extremity movement). In other activities, the HAT should be taken as 127 separate segments. The forces acting on the human are the ground reaction forces and the air frictional forces. 128 There are joint forces and moments acting at the Ankle (A), Knee (K), Hip (H) and Lumbosecral (L) joints. 129 Indicated are the Center of Mass (COM) of each segment, the Center of Pressure of the air friction (CP), where 130 the air frictional force acts upon, and the Center of pressure of the ground reaction force (COP).

4. Mechanical power equations

Before elaborating on the interpretation of mechanical power in the literature, we first set-up the 133 134 complete human mechanical power balance equations (based on the work of Aleshinsky (1986) and van Ingen Schenau & Cavanagh (1990)), to expound the terminology used in this review. The 135 136 equations are based the free on body diagram shown in Figure 2. 137 The human is modelled as a chain of N linked rigid bodies (N \ge 1), where each body is identified as a 138 segment with index i. We start by writing down the power balance of every segment and then add 139 them to come to the power balance for the complete system. For a better understanding of the 140 system behaviour we distinguish between the joint power, which is the mechanical power generated 141 by the human at the joints; the frictional power losses; the kinetic power, which is the rate of change of the kinetic energy; the gravitational power; and the environmental power, which is the mechanical 142 power from external applied forces and moments. We here use the term environmental power to 143 144 avoid confusion, since the term external power has been used to describe several different models 145 (e.g. the change in kinetic energy of the centre of mass (COM), as well as the power measured with a power meter in cycling) (see section 5.2.1). Then, for one segment i we can determine these powers 146 147 from the Newton-Euler equations of motion by multiplying them with the appropriate velocities.

148 Starting with the translational part, the Newton equation, we get for segment i.,

$$\left(\boldsymbol{F}_{j,i} + \boldsymbol{F}_{G,i} + \boldsymbol{F}_{e,i} - \boldsymbol{F}_{f,i}\right) \cdot \boldsymbol{v}_{i} = \boldsymbol{m}_{i} \cdot \boldsymbol{a}_{i} \cdot \boldsymbol{v}_{i}$$
(1)

150 In which $F_{j,i}$ are the joint forces, $F_{G,i}$ are the gravitational forces, $F_{e,i}$ are the external forces, and 151 $F_{f,i}$ are the frictional forces working at the segment (e.g. air friction, ice friction). a_i and v_i are 152 respectively the linear acceleration and velocity of the segment. We write the translational power 153 balance equation as

154
$$P_{j,tr,i} + P_{G,tr,i} + P_{e,tr,i} - P_{f,tr,i} = P_{k,tr,i}$$
(2)

155 Where $P_{j,tr,i}$, $P_{G,tr,i}$, $P_{f,tr,i}$, $P_{e,tr,i}$ are respectively the translational joint power, the translational 156 gravitational power, the translational frictional power, and the translational environmental power. 157 $P_{k,tr,i}$ is the translational kinetic power.

For the rotational power we can take the Euler equation of motion, expressed in the global reference system, and multiply by the angular velocities at the segment, to come to the rotational power equation, as in

161
$$\left(\boldsymbol{M}_{j,i} + \boldsymbol{M}_{e,i} - \boldsymbol{M}_{f,i}\right) \cdot \boldsymbol{\omega}_{i} = \frac{d}{dt} \left(\boldsymbol{I}_{i} \cdot \boldsymbol{\omega}_{i}\right) \cdot \boldsymbol{\omega}_{i}$$
(3)

162 Where $M_{j,i}$ are the joint moments, $M_{e,i}$ are the external moments, $M_{f,i}$ are the frictional moments, 163 and ω_{a} is the segment angular velocity. We write the power as

164
$$P_{j,ro,i} + P_{e,ro,i} - P_{f,ro,i} = P_{k,ro,i}$$
 (4)

165 Next, we add up the rotational and translational segment powers of all segments. The constraint 166 forces in the joints have no contribution to the total power equation, since only relative rotation at 167 the joint between the two segments is assumed (linked segment model), and therefore will drop out

of the equation. Joint forces can redistribute energy between segments and links, but not add energy to the total body system (Aleshinsky 1986). Note however, that if an applied inverse kinematics method allows for translations in the joint, as in Ojeda et al. (2016), or a six degree of freedom joint is applied (e.g., as is possible in biomechanical modelling software such as OpenSim (Delp et al. 2007) and Visual3D (C-Motion,Germantown,MD, USA)), joint forces do play a role and the constraint forces should be accounted for in the power determination (see section 5.1.3).

The total power equations for the system, now written in terms of joint power, kinetic power,frictional power, gravitational power, and environmental power are,

176
$$P_j = P_k + P_f - P_G - P_e$$
 (5)

178 In which we have the joint power (P_i) which is directly calculated using the moments at the joint (

179 M_i) and the rotational velocities around the joint (ω_i), as in

180
$$P_{j} = \sum_{i=1}^{N-1} \boldsymbol{M}_{i,i+1} \cdot (\boldsymbol{\omega}_{i+1} - \boldsymbol{\omega}_{i}) = \sum_{j=1}^{N-1} \boldsymbol{M}_{j} \cdot \boldsymbol{\omega}_{j}$$
(6)

181 We find the gravitational power in equation 5, as in

$$P_G = \sum_{i=1}^N \boldsymbol{v}_i \cdot \boldsymbol{m}_i \cdot \boldsymbol{g}$$
(7)

183 And the frictional power, which consists of translational power and rotational power,

184
$$P_{f} = \sum_{i=1}^{N} \boldsymbol{\omega}_{i} \cdot \boldsymbol{M}_{fr,i} + \sum_{i=1}^{N} \boldsymbol{v}_{i} \cdot \boldsymbol{F}_{fr,i}$$
(8)

185 And the environmental power, which consists of translational power and rotational power,

186
$$P_e = \sum_{i=1}^{N} \boldsymbol{\omega}_i \cdot \boldsymbol{M}_{e,i} + \sum_{i=1}^{N} \boldsymbol{v}_i \cdot \boldsymbol{F}_{e,i}$$
(9)

187 And the change of kinetic energy in the segments,

188
$$P_{k} = \sum \frac{dE_{seg}}{dt} = \sum_{i=1}^{N} \frac{d}{dt} \left(I_{i} \boldsymbol{\omega}_{i} \right) \cdot \boldsymbol{\omega}_{i} + \sum_{i=1}^{N} m_{i} \cdot \boldsymbol{a}_{i} \cdot \boldsymbol{v}_{i}$$
(10)

In summary, the mechanical power balance consists of five parts, joint power, kinetic power, 189 190 gravitational power, environmental power and frictional power. Joint power is generated by the human, and is the result of muscle power. This entails that for the most complete estimation of 191 192 mechanical (human) power either the joint power should be determined directly through measurements of joint torques and angular velocity, or indirectly via the sum of frictional, kinetic, 193 environmental and gravitational power, P_f, P_k, P_e , and P_G (Figure 1). Usually, these powers are 194 195 approximated depending on the available recording methods, and therefore sometimes not all terms 196 in the mechanical power balance are estimated resulting in a simplified model.

197

198 Instantaneous power (IN) versus change of energy (EN)

Power is the amount of energy per unit of time. In the literature there are, apart from the different models, two different approaches to estimate power. First, what is referred to as instantaneous power (IN). Instantaneous power is power at any instant of time, which can be calculated using the power balance equation presented earlier (van Ingen Schenau & Cavanagh 1990). The second approach is by determining the change of kinetic and gravitational energy of a system (EN) over a larger time span, e.g. the cycle time, and divide this energy over the larger Δt . We know that the kinetic energy at time *t* is:

206
$$E_{k,i,t} = \frac{1}{2} \boldsymbol{m} \cdot \boldsymbol{v}_{i,t}^{T} \cdot \boldsymbol{v}_{i,t} + \frac{1}{2} \boldsymbol{\omega}_{i,t}^{T} \cdot \boldsymbol{I}_{i,t} \cdot \boldsymbol{\omega}_{i,t}$$
(11)

207 And the gravitational energy at time *t* :

$$E_{g,i,t} = m \cdot g \cdot y_{i,t} \tag{12}$$

Note that EN only estimates average mechanical power, and does not give insight into the power
development, or peak powers. Also, oscillatory movements will result in a zero outcome with EN (e.g.
walking).

212 5. Power models in the literature

213 Based on the mechanical power equations, we sorted the literature of Search 1-3 concerning the 214 estimation of mechanical power as an indication of mechanical energy expenditure in Tables 1 & 2. 215 For each study the power model $(P_j, P_k, P_f, P_g, P_e)$, the estimation approach (IN, EN) and the 216 dimensions (1D, 2D, 3D) are indicated. Results show that simplifications are done on three scales: 217 the number of bodies (single body vs multibody), the recorded data (kinematic versus kinetic data), 218 and the time interval (IN versus EN). The analysis on results for the literature of Search 4, are given 219 separately in Table 3, divided into articles for single joints versus multi-joints, and work versus power 220 results.

221 5.1 Simplifications of power models

222 5.1.1 Single body models

223 When an athlete is simplified to a single mass, the assumption is that this mass is located at the COM 224 of the full body. Constructing the mechanical power balance (eq. 5) for this single body system results in an equation with one body left, the COM, which automatically neglects any relative 225 226 motions between the segments and the COM, and any power related to these motions. Although this 227 single body approach is used often (27 papers, see Table 1), estimation of the impact of this 228 simplification has only been performed in two studies, both on running (Arampatzis et al. 2000; 229 Martin 1993) et al. 230 Arampatzis et al. (2000) (see also Table 1) compared four mechanical power models in over-ground 231 running at velocities ranging from 2.5-6.5 m/s. Their results showed that the mean mechanical power 232 estimated with the single body model, based on the change in potential and kinetic energy, is 32% 233 higher than the power of the 2D joint power estimation at 3.5m/s running speed. Martin et al. (1993) 234 determined the mechanical power in treadmill running with three methods (see Table 1). Based on 235 their results, a single body kinematic approach resulted in a 47% lower mechanical power estimation 236 compared to joint power, running at 3.35 m/s. Since the neglected frictional power (air friction) at 237 these running speeds is relatively small (<1% of joint power, based on Tam et al. (2012)), the 238 difference between joint power estimation and the kinematic approach for the single body 239 estimation is attributed to the neglected relative motions of the segments to the COM and the fact

Article	Terminology	Dimensions	P _j P _k	P _k	$P_{\rm f} P_{\rm g}$	P _e IN	Comments	Applicable topics from
Single Body models			CNICAL			i		
Running Yanagiya et al. (2003)	Mechanical power	1				X IN	velocity of the belt times the horizontal force on the handle	Directional power (see
Fukunaga et al. (1981) (sprint)	Forward power	2				X IN	Dar	(7.7.5
Pantoja et al. (2016) (sprint)	Mechanical power	1	×		×	NI		
di Prampero et al. (2014) (sprint)	Mechanical accelerating power	1	×		×	IN		
Minetti et al. (2011) (skyscraper)	External power	1			×	EN	Regression for internal power	Internal and external
Gaudino et al. (2013) (soccer)	Mechanical power	1	×			EN		Directional power (see
Arampatzis et al. (2000)	Mechanical power	2				X IN	+14% mean mechanical power ^a	0versimplified model
		2	×		×	EN	[compared to joint power in same experiment, Table 2] +32% mean mechanical power ^b	(see 5.1.1)
Martin et al. (1993)	COM kinematics approach	2	×		×	EN	[compared to joint power in same experiment, Table 2] -47% mean mechanical power ^c	
Bezodis et al. (2015)	External power	1	×			EN	[compared to joint power in same experiment, Table 2]	
Cycling Telli et al. (2017)	External power					X IN		Internal and external
	Additional External power	3	×		×	EN		work (see 5.2.1) Internal and external
Van Ingen Schenau et al. (1992)	External power	1	×		×	EN		power (see 5.2.1)
Swimming Seifert et al. (2010)	External power, Relative power, absolute power	-			×	Z	Fdrag measured: the swimmers swam on the MAD-system, which allowed them to push off from fixed pads with each stroke These push-off pads were attached to a rod which was connected to a force transducer, enabling direct	
Toussaint and Truijens (2005)		-	×		×	I	measurement of push-off forces for each stroke. Assuming a constant mean swimming speed, the mean propelling force equals the mean drag force. Theoretical, not measured	
Toussaint and Beek (1992)		1	×		×	I	Theoretical, not measured	
<i>Rowing</i> Hofmijster et al. (2008) Buckeridge et al. (2012)	External power External power	1 1				NI X X	Integral of handle displacement-handle force curve divided	
Hofmijster et al. (2009)	Internal Power	1	×				Dy LITTIC.	Internal and external
Colloud et al. (2006)	External mechanical power					NI X	Fhandle*vhandle-Fstretcher*vstrechter	power (see 5.2.1)
Speed skating Houdijk et al. (2000a,b)	External power	1			×	EN	About 20% of the joint power consists of Pk + Pg based on van	
de Koning et al. (2005) de Koning et al. (1992) (sprint)	Power output External Power	1	××		××	EN	der Kruk et al. (2018)	

 Table 1

 Structuring of the literature for single body models Indicated are the terminology, the power estimation, the dimensions of the model (1D, 2D, 3D) and whether the power is estimated instantaneously (Instantaneous power (IN)) or via the change in energy over a time span (EN). Inconsistent terminology and oversimplifications are indicated in the final column.

6

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	= 0 %	æ	Internal and external work (see 5.2.1)	Internal and external work (see 5.2.1) Directional power (see 5.2.2)	Oversimplified model (see 5.1.1)	
	<i>rang measured:</i> The drag test setup consisted of a strain gauge force transducer, attached at the front of the treadmil to the front of the wheelchair. Participants were instructed to tremain stationary while the treadmill was raised over a serie of gradients at a constant velocity	<i>Edrag measured</i> : A cable was connected between the wheelchair (standing immobile on a sloped treadmill) and force transducer mounted upon a frame at the front of the treadmill. Fdrag equalled the force needed to prevent the wheelchair from moving backward under influence of belt speed and slope effects.	Theoretical, not measured Regression function		Vertical velocity of the COM x ground reaction force of the bench to the floor	
	EN	EN	EN	Z	N	200%
				×	×	d 4)*1
>	~	×	×			\\Methc
			×) ((Mathod 1- Method 2
Ţ	_	-	1	5	1	
	External Power Output	External power	Internal power	External power, vertical power, horizontal power, lateral power		Table 2 at 3.5 m/s in A Aramatzis et a
Wheelchair	Mason et al. (2011)	Veeger et al. (1991)	Kayaking Jackson (1995) Nakamura et al. (2004)	Sideway locomotion Yamashita et al. (2017)	Bench press Jandacka and Uchytil (2011) (soccer)	^a Based on mean mechanical nower of

^a Based on mean mechanical power of Table 2 at 3.5 m/s in A. Arampatzis et al. (2000); ((Method 1- Method 4)/Method 4)* 100%. ^b Based on mean mechanical power of Table 2 at 3.5 m/s in A. Arampatzis et al. (2000); ((Method 2- Method 4)/Method 4)* 100%. ^c Based on Martin et al. (1993); ((W_{ExCH} in Table 2-TMP in Table 4)/(TMP in Table 4)))* 100%.

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Structuring of the literature for multi body models. Indicated are the terminology, the power estimation, the dimensions of the model (1D, 2D, 3D) and whether the power is estimated directly (Instantaneous power (IN)) or via the change in energy over a time span (EN). Applicable topics from this review are indicated in the last column.

Article	Terminology	Dimensions	P _j P _k	TRANS F	k ROT	Pf P	B Pe	IN /EN	Comments	Applicable topics from this review
Multibody models										
Running										
Willwacher et al. (2013)	Joint power	e	×							
Arampatzis et al. (2000)	Joint power	2	×					N	15 segments	
	Mechanical power	2	×	î	~	~	22	EN	+10% difference in mean mechanical power ^a	
									[compared to joint power in same experiment] 15 segments	
Martin et al. (1993) (sprint)	Joint power	2	×					N	14 segments	
	Segments kinematics	2	×	^	~	~	**	EN	-56% mean mechanical power ^b	
	approach								[compared to joint power in same experiment] 14 segments	
Cycling										
De Groot et al. (1994)	Joint power		×						theoretical	
Neptune and Van Den Bogert (1997)	Joint power	2	×					N		
	Internal and external power	2	×	î	~	××		N		Internal and external work (see 5.2.1)
Telli et al. (2017)	Internal power	3	×	Ŷ	~			EN	Relative to COM	Internal and external work (see 5.2.1)
Golf McNally et al. (2014)	Joint power	m	×							
Walking Royer and Martin (2005)	Mechanical work	2	×	Â	~	~		EN		

^a Based on mean mechanical power of Table 2 at 3.5 m/s in A. Arampatzis et al. (2000); (Method 3-Method 4/Method 4) * 100%. ^b Based on Martin et al. (1993): ((*W_{WB}*in Table 3-TMP in Table 4)/(TMP in Table 4))) * 100%.

used to estimate mail correlated sector with the acrosse demand of

Articles found with the search terms joint pr (joint power was taken over multiple joints, negative work are separated. Articles are so	ower and sport.). Noted are the orted on year of	The literature was divided into estimating power or applied inverse dynamics technique with reference publication.	work of a single joint (the research esti (N.M. = not mentioned). For the work e	nated the joint power of individual joints), and power and w stimation, the conversion from power to work is given and	ork of multiple joints whether positive and
Joint power					
Power per joint	Movement	Inverse dynamics method			
Paquette et al. (2017)	Running	"Newtonian inverse dynamics"	N.M.		
Middleton et al. (2016)	Cricket	"Standard inverse dynamics analysis"	N.M.		
Barratt et al. (2016) Darratt af (2016)	Squate	inverse dynamics method N M	Elitman (1939) N M		
	jumps	TATA T			
Van Lieshout et al. (2014)	Exercises	N.M.	N.M.		
Creveaux et al. (2013)	Tennis	[Method is fully described in paper]	n.a.		
Kuntze et al. (2010)	Badminton		N.M.		
Dumas and Cheze (2008)	Gait	"Inverse dynamics based on wrenches and	Dumas et al. (2004)		
		quaternions"			
Vanrenterghem et al. (2008)	Jumping	N.M.	N.M.		
Schwameder et al. (2005)	Walking	"Standard 2D inverse dynamics routine"	N.M.		
Jacobs and van Ingen Schenau (1992)	Sprint	New contait equations of incuron "Linked segment model"	N.M. Elftman (1939)		
Energy per Joint	Movement	Inverse dynamics method		Power to work	Absolute
Schache et al. (2011)	Running	"A standard inverse dvnamics technique"	Winter (2009)	integral of ioint power over time	Not absolute
~	0	-	~		(pos and neg
(110C) In the Himmell	Dunning	"docomer of mention of the second sec		NN	WOrk) Not sheetute
	giiiiiny	Newton-Eurel Inverse dynamics approach	TAT.VI	. IA. N	(pos and neg
	-				work)
SOTENSON ET AL. (2010)	dunf	inverse Dynamics	VISUAL 30	integral of joint power over time	Not absolute (pos and neg
Yeow et al. (2010: Yeow et al. 2009)	Landing	N.M.	N.M.	Integral of joint power over time	work) Not absolute
	jump			-	(pos and neg work)
Power multiple joints	Movement	Inverse dynamics method			
Strutzenberger et al. (2014)	Cycling	"Sagittal plane inverse dynamics"	Visual 3D	Integral of the summed ankle, knee, and hip powers	I
Energy multiple joints	Movement	Inverse dynamics method		Power to work	Absolute
Greene et al. (2013, 2009)	Rowing	Custom program	Winter (2009)	Sum of the joint mechanical energy	N.M.
Attenborough et al. (2012)	Rowing	Inverse dynamics	Winter (2009)	Integration of the absolute value of the power time	Absolute per
Lees et al. (2006)	Jumping	"Inverse dynamics using standard procedures"	Miller and Nelson (1973), Winter	Time integral per joint "Standard procedure', de	Not absolute
			(2009)	Koning and van Ingen Schenau (1994); sum of left and right limb:	(pos and neg work)
Devita et al. (1992)	Running	"An inverse dynamics method"	N.M.	Resultant joint powers around hip, knee and ankle joint were summed at each time point.	Not absolute (pos and neg
					work)

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that only measured kinematic data were used in the single body, which is expected to be less accurate than the combination of measured force and kinematic data. The difference in results between the two studies is surprising, since the mechanical equations, running speeds, and joint power models (14 versus 15 segments, 2D, absolute per joint) are similar for both studies, while the only difference was the treadmill versus over-ground condition. Unfortunately, Arampatzis et al. (2000) do not discuss this difference.

246 It is clear that, although there is no consensus on whether a single body model under- or 247 overestimates the mechanical power in running (see also section 5.2.1), both studies show significant 248 differences between a single body model and a joint power model. Since this is the consequence of 249 disregarding the motions of the segments and kinematic measurement accuracy, validity will likely be 250 different for different movements.

251 Three studies were found that determined the mechanical power in locomotion with a single body 252 model by multiplication of an environmental force (e.g. the measured ground reaction forces) times 253 the velocity of the centre of mass of the complete body (Arampatzis et al. 2000; Yamashita et al. 254 2017; Jandacka & Uchytil 2011). Theory of this model lays in the simplification of an athlete to one 255 rigid body being propelled by a force. Therefore, the ground reaction force, which acts on the foot is 256 now shifted to the COM and assumed to cause the movement of the complete (rigid) body. However, 257 although a force can be replaced by a resultant force acting at the COM without changing the motion 258 of the system, the work of the system will divert from the actual work. For example, the ground 259 reaction force in running, acting on the foot, in principle hardly generates power, after all the foot 260 has close to zero velocity (Zelik et al. 2015). By assuming that the force acts on the COM of the 261 athlete, the force suddenly generates all power (and therefore work). So although mechanically, with the rigid body assumption, the simplified model is in balance, the validity of modelling an athlete as a 262 263 point mass (single body) driven by the ground reaction force is highly doubtful. The results of such a 264 model should in no case be interpreted as an indication of muscle power/work or MEE, since the 265 relationship with actual joint power is lost by the oversimplification of an athlete.

266 For single body power estimations, both IN approaches (e.g. Pantoja et al. 2016; di Prampero et al. 267 2014; Seifert et al. 2010) and EN approaches (e.g. Minetti et al. 2011; Gaudino et al. 2013; Houdijk et 268 al. 2000) were found. An EN approach results in an average mechanical power estimate. 269 Consequently, there is no insight into the course of power during the motion cycle, e.g. peak power. 270 Also, oscillatory motions are averaged such that positive and negative power would negate each 271 other, which are tricky assumptions for several sports like running, cycling, swimming, etc. Van der 272 Kruk (2018) found that the kinetic and gravitational power related to these oscillatory motions in 273 speed skating (zig-zag motion of the skater over the straight), appeared to account for almost 20% of 274 the joint power. Therefore, assumptions on ignoring velocity fluctuations, or motions that do not 275 directly contribute in the forward motion, should be well validated. Especially when working with 276 top-athletes or highly technical sports, these components could be the key-factors in an athlete's 277 performance, therefore IN models seem more appropriate than EN models for understanding 278 performance (Caldwell & Forrester 1992).

279 5.1.2 Multibody models

Using a multi-body approach is much more complex than the single body approach, since the motion of the separate body parts needs to be measured. The benefit of this approach is that the power per segment gives insight into the distribution of power over the body. In the *kinematic approach*, only recorded kinematic data are used to indirectly estimate mechanical power: frictional power, kinetic power and gravitational power (P_f , P_k and P_G). The main difference with the joint power estimation, is the absence of measured force data. Furthermore, in the kinematic approach frictional power is neglected in running and walking studies, and gravitational power in cycling studies.

287 The studies by Arampatzis et al. (2000) and Martin et al. (1993), which were mentioned earlier, enable the comparison of a kinematic multi-body approach, which resulted in respectively 10% more 288 289 mechanical power and 56% less mechanical power when compared to the joint power estimation (at 290 respectively 3.5 m/s and 3.35 m/s) (Table 2). Again, their results are contradictory and largely diverge 291 in magnitude. However, the results do stress the need of accurate kinematic measurements in the 292 models. The approaches in which both recorded kinematic and force data were used to estimate 293 MEE correlated better with the aerobic demand of the athletes than the kinematic data only 294 approaches (Martin et al. 1993).

295 *5.1.3 Joint power*

Since we found several inconsistencies in estimating joint power in the articles of *Search 1-3* (see Table 2), we performed a specific search for joint power (*Search 4*). Analysis of these studies lets us identify two classes of differences in joint power estimation: the inverse dynamics method (including the degrees of freedom of the joints) and the estimation of power to work (see Table 3).

300 Joint power estimation requires the determination of joint moments and forces via an inverse 301 dynamics method. Although several methods exist to estimate joint moments (e.g. Dumas et al. 302 2004; Kuo 1998; Elftman 1939), the bottom-up approach (Winter 2009; Elftman 1939; Miller & 303 Nelson 1973) is still the most applied method, and referred to as the 'standard inverse dynamics 304 method' or 'Newton(-Euler) inverse dynamics approach' without citing further reference. However, 305 since the bottom-up approach can leave large residuals at the trunk and the joint power is largely 306 influenced by the inverse dynamics method (up to 31% (van der Kruk 2018)), there should be more 307 attention towards this part of the power estimation.

308

309 Underlying the inverse dynamics is the choice for the kinematic model, where we mainly found 310 differences in the degrees of freedom of the joint (van der Kruk et al. 2018). If translation is allowed 311 in the joints, the joint forces suddenly generate power (see eq. 2). Application of 6 DOF joints, and 312 therefore incorporation of translational joint power is becoming more common, due to the ever 313 more detailed 3D human joint models (e.g. OpenSim, Visual3D). The effect of these forces on the 314 joint power, and whether the translations are not part of residuals of the choice in inverse kinematics 315 method, rather than a physiological phenomenon, falls outside of the scope of this review (Ojeda et 316 al. 2016; Zelik et al. 2015). However, we want to make the reader aware that differences do occur 317 and thereby influence the joint power estimations, where the increase in complexity will not 318 automatically imply improvement.

319

320 The second class of difference was found in the integration of joint *power to work* (as indication of 321 MEE). For the power in a single joint, a separation is made between *negative and positive power*. 322 Negative power occurs when the moment around the joint is opposite to the angular velocity of the 323 joint, which would denote braking (dissipation of energy). With only mono-articular muscles, this 324 would imply the production of eccentric power. However, bi-articular muscles can 'transfer' power to 325 adjacent joints. Converting power into work is done by taking the integral of the power curve over 326 time. In the literature, the division is made between *positive work* and *negative work* (Schache et al. 327 2011; Yeow et al. 2009; Hamill et al. 2014; Sorenson et al. 2010). This division is made since, from a 328 biomechanical perspective, it is assumed that for negative muscle work (or eccentric muscle 329 contraction) the metabolic cost is lower than for positive muscle power requiring concentric muscle 330 contraction. However, there is no general consensus on the exact magnitude of this difference. Caldwell & Forrester (1992) even argue that the division into positive and negative work should be 331 332 rejected, since mechanical power is an indication of muscle power, not metabolic cost and thus 1 J of 333 negative power reflects 1 J of positive power. However, currently the general consensus is to separate negative from positive work; musculoskeletal simulations might shed light on the differencein magnitude in the future.

336

For power estimation in multiple joints, the estimation of mechanical work (indication of MEE) 337 338 becomes more complicated due to the *power flow* between segments (and thus joints); bi-articular 339 muscles activations can induce both negative and positive power simultaneously around adjacent joints (Van Ingen Schenau & Cavanagh 1990). When no power flow is assumed, the integral of the 340 341 absolute joint power per joint is taken and summed over the joints (Attenborough et al. 2012). If 342 power flow is assumed, the joint powers are first summed over the joints and then the integral over 343 time is taken, again allowing for the separation of negative and positive power (Lees et al. 2006; 344 Devita et al. 1992). What the best approach is, has yet to be determined. Hansen (2003) found in 345 cycling that the MEE was most accurately measured with a model that allowed for energy transfer 346 only between segments of the same limb. Articles that do not report the method for MEE estimation are inappropriate for comparison (e.g. Greene et al. 2013), since the difference between the two 347 348 methods can go up to >2.5x the MEE (measured in running (Martin et al. 1993). Note that this power 349 flow issue not only accounts for the estimation of joint power over several joints, but also for power 350 transfer between segments in other kinematic multi-body models (Willems et al. 1995).

- 351 [Table 3]
- 352

353 5.2 Inconsistent terminology



354

355 *Figure 3* Free body diagram of a two-link segment body

356 5.2.1 Internal and external work

The terms internal and external power and work are often used. However, these terms are illdefined, terminology is inconsistent, and the actual purpose of separation is dubious. We will discuss these issues by considering a simple 2D two-link model (Figure 3). The mechanical power equations of this simple model can be divided into external powers and internal powers. We here employ the definition of internal power as the energy changes of the segments, relative to the COM of the complete body (Aleshinsky 1986). The power equation for this model can be divided as follows:

$$\frac{dE}{dt} = \left[\frac{d}{dt} \left\{ \frac{M \cdot (\dot{x}_{com}^{2} + \dot{y}_{com}^{2})}{2} + M \cdot g \cdot y_{com} \right\} + \frac{d}{dt} \left\{ \sum_{i=1}^{N} \left[\frac{m_{i} \cdot (\dot{x}_{ci/com}^{2} + \dot{y}_{ci/com}^{2})}{2} + \frac{I_{ci} \cdot \dot{\phi}_{i}}{2} \right] \right\} = \frac{1}{F_{o}^{x} \cdot \dot{x}_{com} - F_{d}^{x} \cdot \dot{x}_{com} + F_{o}^{y} \cdot \dot{y}_{com}} + F_{o}^{x} \cdot \dot{x}_{o/com} + F_{o}^{y} \cdot \dot{y}_{o/com} + \left[\sum_{i=1}^{N-1} M_{1,2} \cdot (\dot{\phi}_{2} - \dot{\phi}_{1}) \right] + M_{o} \cdot \dot{\phi}_{1}}$$

(13)

363

in which the parts in the blue boxes represent the external powers, and the parts in the green boxes the internal powers. Note that the external force F_o acts at o, and:

366
$$\dot{x}_{o} = \dot{x}_{com} + \dot{x}_{o/com}; \ \dot{y}_{o} = \dot{y}_{com} + \dot{y}_{o/com}$$
 (14)

Although these equations show that the system energy can be presented as a sum of external and internal power, the mechanical work is *not equal* to the sum of the 'internal' and 'external' work (Zatsiorsky 1998; Aleshinsky 1986). Take into consideration that:

370
$$\dot{x}_{com} = \dot{x}_o - \dot{x}_{o/com}; \ \dot{y}_{com} = \dot{y}_o - \dot{y}_{o/com}$$
 (15)

371 If we then determine mechanical work by taking the absolute integral of the power equations 372 separated into internal and external power, we obtain:

$$\begin{bmatrix}
T_{1}^{2} \\
\frac{d}{dt} \left\{ \frac{M \cdot (\dot{x}_{com}^{2} + \dot{y}_{com}^{2})}{2} + M \cdot g \cdot y_{com} \right\} dt + \int_{T_{1}}^{T_{2}} \left| \frac{d}{dt} \left\{ \sum_{i=1}^{N} \left[\frac{m_{i} \cdot (\dot{x}_{cilcom}^{2} + \dot{y}_{cilcom}^{2})}{2} + \frac{I_{ci} \cdot \dot{\phi}_{i}}{2} \right] \right\} dt \neq \\
373 \qquad \begin{bmatrix}
T_{1}^{2} \\
F_{o}^{x} \cdot \dot{x}_{o} - F_{d}^{x} \cdot \dot{x}_{com} + F_{o}^{y} \cdot \dot{y}_{o} - F_{d}^{y} \cdot \dot{y}_{com} - F_{o}^{x} \cdot \dot{x}_{olcom} - F_{o}^{y} \cdot \dot{y}_{olcom} \right| dt + \\
\begin{bmatrix}
T_{1}^{2} \\
F_{o}^{x} \cdot \dot{x}_{olcom} + F_{o}^{y} \cdot \dot{y}_{olcom} + \left[\sum_{i=1}^{N-1} M_{1,2} \cdot (\dot{\phi}_{2} - \dot{\phi}_{1}) \right] + M_{o} \cdot \dot{\phi}_{1} dt
\end{bmatrix}$$
374 (16)

375 As mentioned by Aleshinsky in 1986, there are external forces (F_a) inside the 'internal' work, 376 therefore the internal and external work are not independent measures. Moreover, the absolute 377 values (due to positive and negative work) destroy the balance. Members of the expressions in the 378 internal and external work are powers which regularly fluctuate out of phase, thereby cancelling 379 each other out. By treating them as independent measures, the work doubles instead of cancelling 380 out, while in reality these powers do not cost any mechanical energy (e.g. pendulum motion). Replacing an actual system of forces applied to a body by the resultant force and couple does not 381 382 change the body motion. It can change, however, the estimation of performed work. Therefore, the 383 power of the external forces as a hypothetical drag force, when assumed this acts at the COM, can be 384 seen separate from the internal power (there is no relative velocity between the point of application 385 of the force and the COM). However, ground reaction forces, or any other forces with a point of 386 application different from the COM will be part of both the 'internal' and 'external' work, and 387 therefore are not independent measures (see also section 5.1.1). 388 Despite the mechanical incorrectness of the separation of internal from external work, and the discussion involving these measures (Zatsiorsky 1998; van Ingen Schenau 1998), more recent 389 390 publications still make this distinction (e.g. Minetti et al. 2011; Nakamura et al. 2004), raising the 391 question what the benefit is of separating the mechanical energy into internal and external energies 392 if the separation is mechanically incorrect? In cases where the whole mechanical power balance is 393 estimated, there seems no point in dividing the power into internal and external power or work. This 394 separation has not given additional useful insight into human power performance in sports so far. 395 The only application of the separation could be when a single body model is used and therefore only 396 external power can be measured. The balance ratio between internal and external power can then 397 used to the consequences of the be provide insight into simplification. 398 Adding to the confusion of the interpretation of external and internal power, is the inconsistent use 399 of the terms. The use of the term 'internal' is logically diffuse, while it might refer to muscular or 400 metabolic work (Williams 1985). In this literature review, two articles were found that used the 401 internal power for estimations different from the definition given above, defining internal 402 mechanical power loss as the part of power absorbed by the muscles that is lost to heat (estimated 403 as fluctuations in kinetic energy of the back and forth moving of the rower on an ergometer) 404 (Hofmijster et al. 2009), or the total energy required to move segments (Neptune & Van Den Bogert 405 1997). However, more models and interpretations of internal power have been published, that all 406 differ power output estimation largely (up to 3x) in (Hansen et al. 2004). 407 Also the term external power is inconsistently used. Aleshinsky (1986) defined the term as the 408 change in energy of the COM of the athlete, and can therefore be seen as a single body model. The 409 origin of the term lies in the assumption that the human generates power only to overcome external 410 forces (e.g. air friction, ground friction). In speed skating (Houdijk et al. 2000; de Koning et al. 1992), 411 wheelchair sports (Veeger et al. 1991; Mason et al. 2011) and swimming (Seifert et al. 2010), the 412 term external power is used for the estimation of frictional power (P_f), assuming that, under constant 413 velocity, this is equal to the power generated by the human. In rowing (Hofmijster et al. 2008; 414 Buckeridge et al. 2012; Colloud et al. 2006) and cycling (Telli et al. 2017), where ergometers are 415 available, the term external power is used to describe the power output measured by the ergometer, 416 what we define as environmental power (P_e). Note however, that the power output measured with 417 an ergometer or a system such as SRM is not necessarily the same as the COM movement. If a cyclist 418 stops pedalling on an ergometer but moves her or his upper body up and down, there is a COM 419 movement (due to joint power), but there is no power measured at the ergometer (P_e) (the cyclist of 420 course does not have to stop pedalling for the same effect). In running and walking, where the 421 frictional power is only marginal and environmental power in principle is zero, the term external 422 power is used to describe the change in kinetic energy (P_k) (Bezodis et al. 2015) and/or gravitational 423 energy (Pg) (Minetti et al. 2011) of the COM, but also for an estimation done by multiplication of the 424 ground reaction forces times the COM velocity (see section 5.1.1 on the reliability of this model). 425 More interpretations of external power can be found in Table 1. 426 So even though the term external power is well known and frequently used, the estimation is not 427 straightforward and interrelations are not always clear. The terms internal and external power can, 428 however, be structuralized and classified by the mechanical power balance from section 3, as was 429 done in Table 1 and 2. We propose a standard in section 6.

430 5.2.2 Directional power

In the studies on running and walking, we found many power terms related to some sort of direction: forward power, lateral power, etc. (see Table 1 and 2). Since power is a scalar, it is in principle incorrect to give the power a certain direction, although of course the forces and velocities related to power have a direction. The separation of the mechanical power equations into these different directions is actually not beneficial. Take for example a situation where there is no environmental power acting on the human e.g. walking; in that situation the power equation simplifies to:

$$\begin{array}{l} 437 \qquad \frac{d}{dt} \left\{ \frac{M \cdot \left(\dot{x}_{com}^2 + \dot{y}_{com}^2 \right)}{2} + M \cdot g \cdot y_{com} \right\} + \frac{d}{dt} \left\{ \sum_{i=1}^{N} \left[\frac{m_i \cdot \left(\dot{x}_{ci/com}^2 + \dot{y}_{ci/com}^2 \right)}{2} + \frac{I_{ci} \cdot \dot{\phi}_i}{2} \right] \right\} = \left[\sum_{i=1}^{N-1} M_{1,2} \cdot \left(\dot{\phi}_2 - \dot{\phi}_1 \right) \right] \right\}$$

(17)

Although the translational left side of this equation can be divided into terms related to a certain translational direction, the eventual power production, on the right side of this equation, cannot be separated into these directions. Separating the left side of the equation into directional terms, is completely dependent on the chosen global frame; moreover, 'vertical' power can very easily be

translated into a 'lateral power' without adding power to the system, e.g. due to centrifugal forces.

444 5.3 E-gross

445 This review clearly showed that there arise large differences in mechanical power estimation based 446 on the choice for a model. These differences also impact research studies which estimate metabolic 447 power with gross efficiency calculations (e-gross), which is the ratio between the expended work 448 (metabolic work) and the performed work (mechanical work). E-gross is often determined in a lab, 449 using VO₂-measurements, to convert mechanical work into energy expenditure. Main causes in the 450 differences among athletes and inaccuracies in measurement of e-gross have been ascribed to the 451 metabolic side of the equation. However, determination of the mechanical power with simplified models influences the e-gross estimation evenly well. When only part of the mechanical power 452 453 balance is determined, for example with a single body model, the dependency of e-gross to the 454 relative movements of the segments is neglected (e.g. de Koning et al. (2005)). If an athlete would 455 then change movement coordination (technique) between the submaximal experiment (where e-456 gross is set) and the actual experiment, the change in segment motion is neglected in the mechanical 457 power and thus in the metabolic power estimation. Especially for technique dependent sports (e.g. 458 swimming, speed skating), this seems an important fact.

459 **6. Discussion**

460 This review provided an overview of the existing papers on mechanical power in sports, discussing 461 the application and the estimation of mechanical power, the consequences of simplifications, 462 mechanically inconsistent models, and the terminology on mechanical power. Structuring the 463 literature shows that simplifications in models are done on four levels: single vs multibody models, 464 instantaneous power (IN) versus change in energy (EN), the dimensions of a model (1D, 2D, 3D) and 465 neglecting parts of the mechanical power balance. Except for the difference between single versus 466 multibody models in running, no studies were found that quantified the consequences of simplifying 467 the mechanical power balance in sport. Furthermore, inconsistency was found in joint power 468 estimations between studies in the applied inverse dynamics methods, the incorporation of 469 translational joint power, and the integration of joint power to energy. Both the validation on 470 simplification of models and the lack of a general method for joint power or work are research areas 471 well worth investigating.

472 The terms internal power and external power/work are, apart from the discussion on the actual 473 usefulness of this power separation, confusing, since several meanings were attributed to the terms. 474 The interrelations between the different interpretations of external power have been discussed here. 475 Based on the above, we suggest that it might be more clear to use the terms from the mechanical 476 power balance: joint power (eq. 6), gravitational power (eq. 7), frictional power (eq. 8), 477 environmental power (eq. 9) and kinetic power (eq. 10) and not use the terms internal and external 478 power or work. In case the power due to motion of the COM and due to motion of the segments 479 relative to the COM are to be separated for measurement conveniences, we propose to work with 480 the term Peripheral Power for moving body segments relative to the COM (Zelik & Kuo 2012; Riddick 481 & Kuo 2016). Note however, that these should not be interpreted as separate energy measures 482 (mechanical work). The awareness that terms internal and external work/power are not self-evident 483 and therefore need explanation and interrelation to the mechanical power balance, will reduce the 484 possibility of errors and increase the comprehension for the reader. 485 To quote Winter et al. (2016): ' if sport and exercise science is to advance, it must uphold the 486 principles and practices of science.' This review only revealed the tip of the iceberg of the studies 487 concerned with estimating 'power' in sport (the search term power and sport results in 9,751 articles 488 (August 2017)), but illustrates clearly that the sport literature would benefit from structuring and 489 validating the research on (mechanical) power in sports. By structuring the existing literature, we 490 identified some obstacles that may hamper sport research from making headway in mechanical 491 power research.

492 7. Conclusions

493

- 494 Performance is not a direct translation of mechanical power. •
- 495 Mechanical power is not a direct estimation of muscle power. Mechanical work is also no • 496 direct measure of energy expenditure for movement.
- 497 Mechanical power is estimated via the joint power directly, or via the sum of kinetic, • 498 frictional, gravitational and environmental power; all other estimations are simplifications.
- 499 Due to limitations in human motion capture in sports, simplified models are employed to ٠ 500 determine power. Simplifications in models are done on four levels: single vs multibody 501 models, instantaneous power (IN) versus change in energy (EN), the dimensions of a model 502 (1D, 2D, 3D) and neglecting parts of the mechanical power balance.
- 503 Single body models by definition neglect the relative motion of the separate body segments • 504 to the COM of the body. The resulting underestimation in power, as an indication of muscle 505 power, is rarely determined in sports, whereas this part of power is an essential part of the 506 mechanical power balance in technique driven sports as e.g. speed skating, swimming or 507 skiing.
- 508 IN models are more appropriate than EN models for understanding performance of elite • 509 athletes. EN automatically results in determination of average power and therefore 510 oscillatory movements are averaged such that positive and negative power would negate 511 each other.
- 512 Little attention is given to the chosen inverse dynamics technique to estimate joint moments ٠ 513 and forces, although its influence on joint power estimation is large (e.g. 31% in speed 514 skating).
- 515 When 6DOF joints are applied (e.g. OpenSim, Visual3D), joint forces not only distribute 516 energy, as in the classical 3DOF joint rotational models, but also allow for translational 517 power; Sport researchers should be aware of the differences between these joint power 518 estimations.
- 519 There is no consensus on how negative and positive work in a single joint should be summed. ٠ 520 On the same note, there is no standard on whether to allow for energy flow between joints. 521 The chosen approach is not always clear from the articles, although factors of 2.5x difference 522 between approaches have been found.
- 523 The terms external and internal power and work are inconsistent. The terms can easily be • 524 replaced by the terms joint power, kinetic power, gravitational power, frictional power and 525 environmental power mentioned in the mechanical power balance of this review paper, 526 which will avoid future confusion.
- 527 • Gross-efficiency (e-gross) is not constant within and between athletes. Apart from metabolic 528 causes, this can also be caused by the procedure of mechanical power determination.
- 529

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